

ORBUMP Power Supply Design Review

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P.S. Load Physical Description

- Three (3) magnets in series – parallel configuration
- Single magnet inductance = $1.8 \mu\text{H}$ (measured)
- Single magnet dc resistance = $34 \mu\Omega$ (calculated)
- Total load inductance = $2.7 \mu\text{H}$
- Total load resistance = $51 \mu\Omega$
- Short stripline with maximum inductance of 40 nH
- Total of twenty (20) RG 220 cables in parallel, 75 ft long maximum

P.S. Current Requirements

- Nominal pulse amplitude = 15 kA
- Maximum pulse amplitude = 17.5 kA
- Maximum flat top duration = 50 μ sec.
- Pulse flatness = $\pm 0.5\%$
- Rise time
 - Minimum = 30 μ sec.
 - Maximum = 40 μ sec.
- Fall time
 - Minimum = 30 μ sec.
 - Maximum = 40 μ sec.

P.S. Current Requirements, cont.

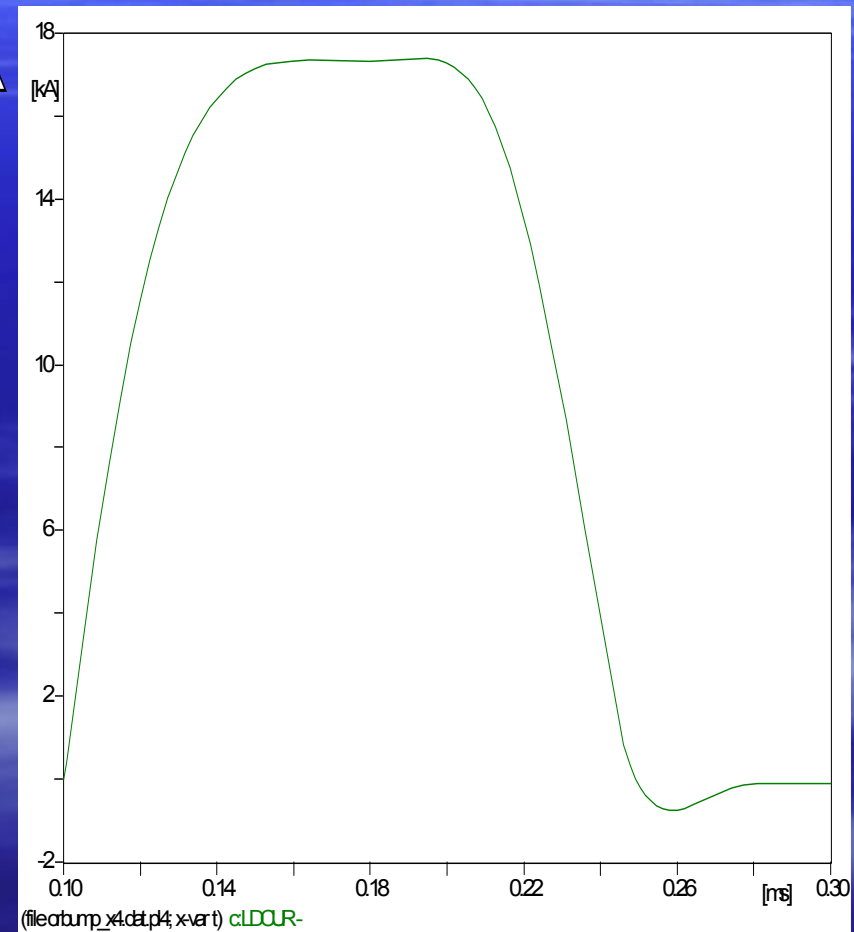
- Nominal repetition rate = 15 Hz
- Pulse repeatability = $\pm 1\%$
- Undershoot
 - Maximum amplitude = 5%
 - Minimum duration = 10 μsec .

Power Supply Design Criteria

- Use Ken's new SCR switch
- Utilize as many MP01/MP02 elements as possible
- Utilize existing PFN inductors
- Fit existing ORBUMP power supply space and utilities
- Use line harmonic reduction equipment

Power Supply Current

- Pulse amplitude = 17.5 kA
- $I_{\text{rms}} = 672 \text{ A}$
- Rise time (10% - 90%) = 33 μs
- Fall time (90% - 10%) = 36 μs
- Flatness = $\pm 0.27\%$
- Pulse width = 50 μs



Switch Assembly

- 5 parallel switches
- 3 SCRs in series each
- CT monitoring total current
- Switch is assembled and tested
- 5 spare individual switches assembled and tested



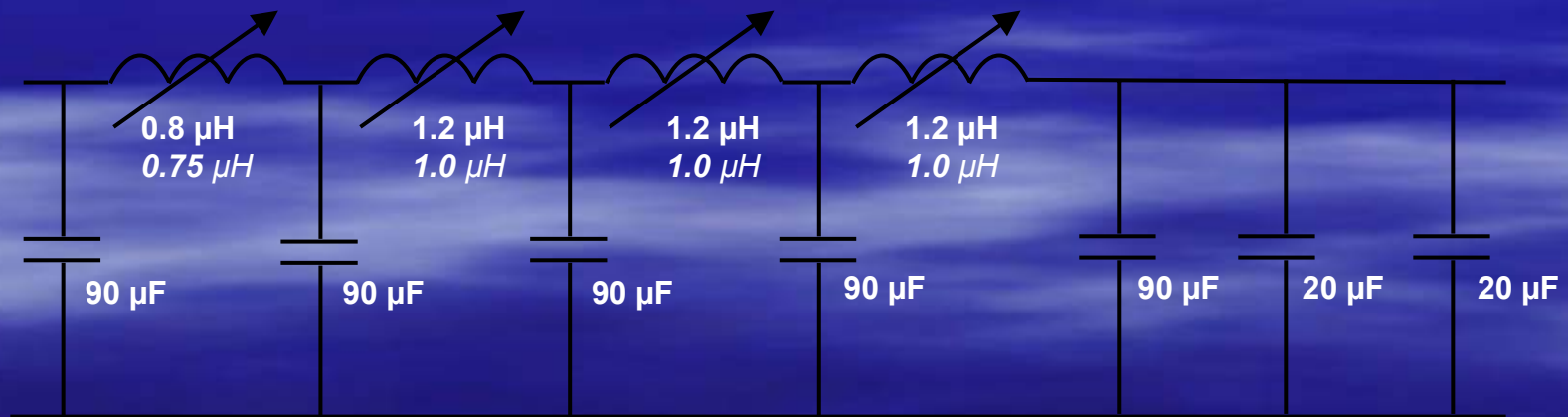
Charging Power Supplies

- Four MP01/MP02 style charging power supplies needed
- Each supply is rated 3 kV, 6 A
- Need 2.05 kV, 3.35 A each



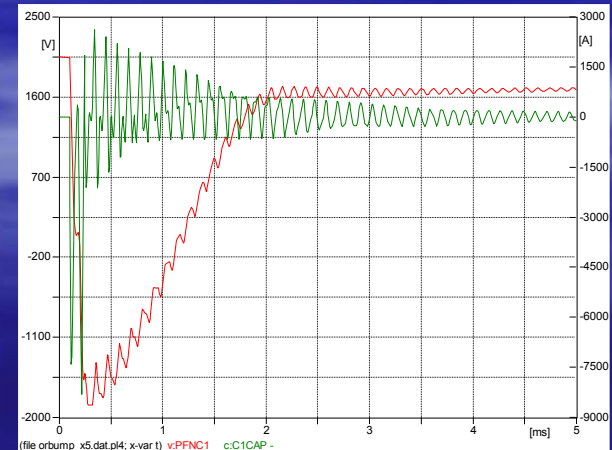
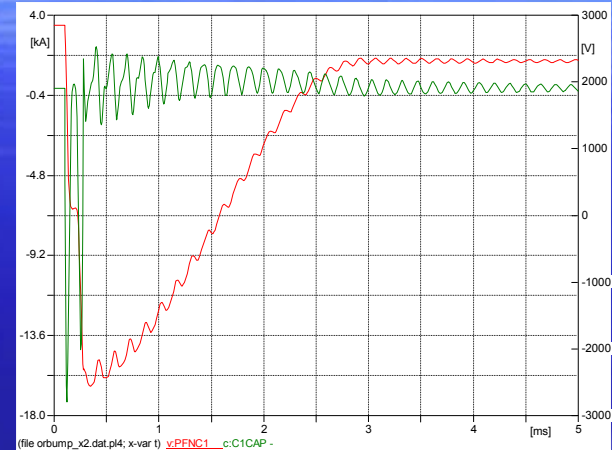
PFN

- 8% coupling between adjacent inductors (diagram below)
- 0% coupling simulated gave same results (inductor self inductance in *italic*)
- Additional capacitors to improve rise time
- Coupling measurements planned



PFN Capacitors

- Available:
 - Capacitance = $180\ \mu\text{F}$ (2 x $90\ \mu\text{F}$)
 - Voltage = $\pm 2.85\ \text{kV}$
 - Discharge Current
 - Peak = $17.2\ \text{kA}$
 - Rms = $500\ \text{A}$
- EMTP Simulations:
 - Capacitance = $90\ \mu\text{F}$
 - Voltage = $\pm 1.86\ \text{kV}$
 - Discharge Current
 - Peak = $8.3\ \text{kA}$
 - Rms = $250\ \text{A}$



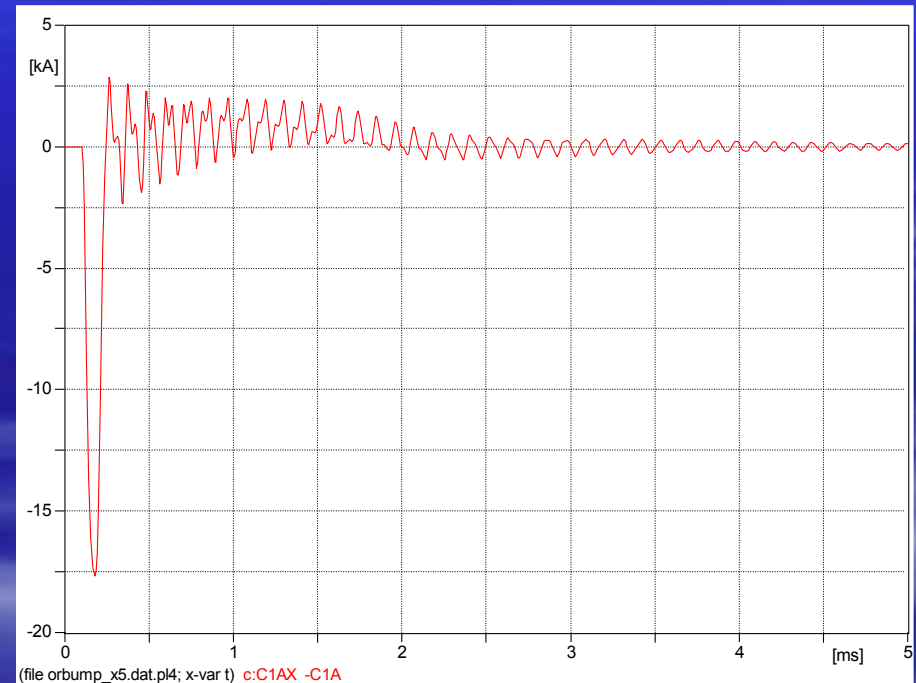
PFN Inductors

■ Simulations:

- $L = 0.8 - 1.2 \mu\text{H}$
- Current
 - Peak = 17.7 kA
 - Rms = 575 A

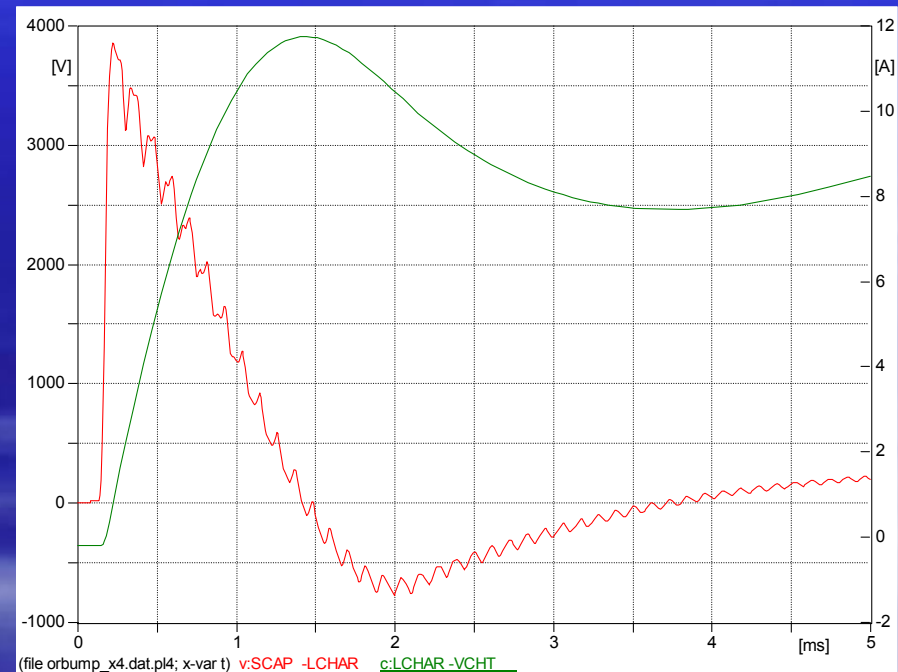
■ Existing Inductors:

- $L = 0.1 - 4.0 \mu\text{H}$
- $Q = 1 - 6$ (1 kHz)
- Conductor size = 420 MCM
- Water flow = 1.5 GPM
- Current
 - Peak = 40 kA
 - Rms = 1.37 kA



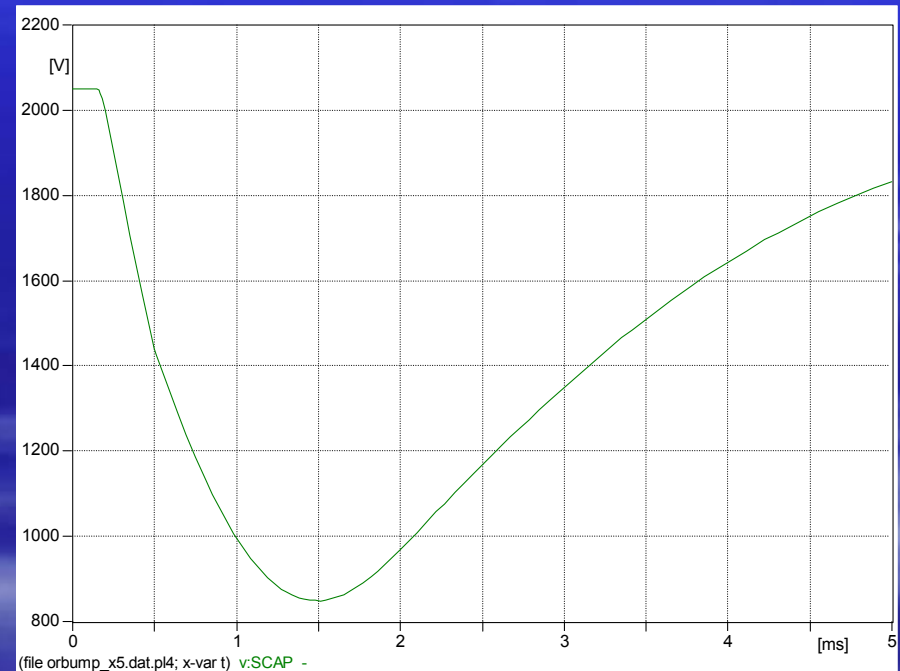
Charging Choke

- Simulations:
 - $L = 0.2 \text{ H}$
 - $V = 3.85 \text{ kV}$
 - Charging Current
 - Peak = 13 A
 - Rms = 10 A
- MP01/MP02 choke:
 - $L = 0.2 \text{ H}$
 - $V = 5 \text{ kV}$
 - Charging Current
 - Peak = 80 A
 - Rms = 20 A



Charging Capacitor

- Available:
 - $C = 20 \mu\text{F}$
 - $V = 2,85 \text{ kV}$
 - Current
 - Peak = 1 kA
 - Rms = 20 A
- Simulations:
 - $C = 20 \mu\text{F}$
 - $V = 2.05 \text{ kV}$
 - Current
 - Peak = 11.7 A
 - Rms = 7 A



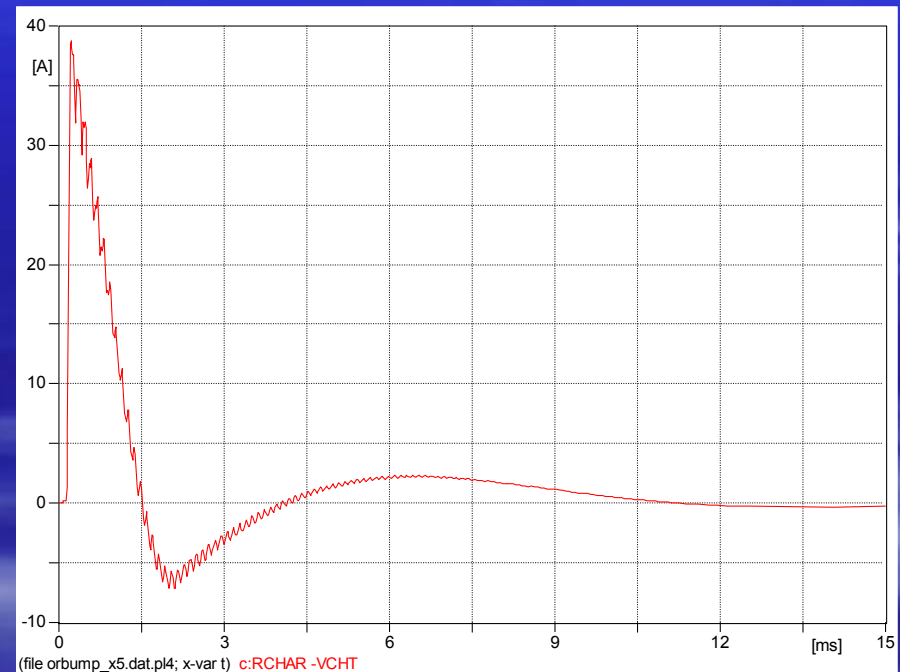
Charging Resistor

■ Simulations:

- $R = 100 \, \Omega$
- $V = 3.85 \, \text{kV}$
- $I_{\text{rms}} = 1.6 \, \text{A}$
- $P = 256 \, \text{W}$

■ Available:

- $R = 100 \, \Omega$
- $V = 8.9 \, \text{kV}$
- $I_{\text{rms}} = 3.2 \, \text{A}$
- $P = 1000 \, \text{W}$



Charge Recovery Choke

■ Simulations:

- $L = 0.8 \text{ mH}$

- $V = 1.8 \text{ kV}$

- Current

 - Peak = 1.3 kA

 - Rms = 155 A

■ MP01/MP02 choke:

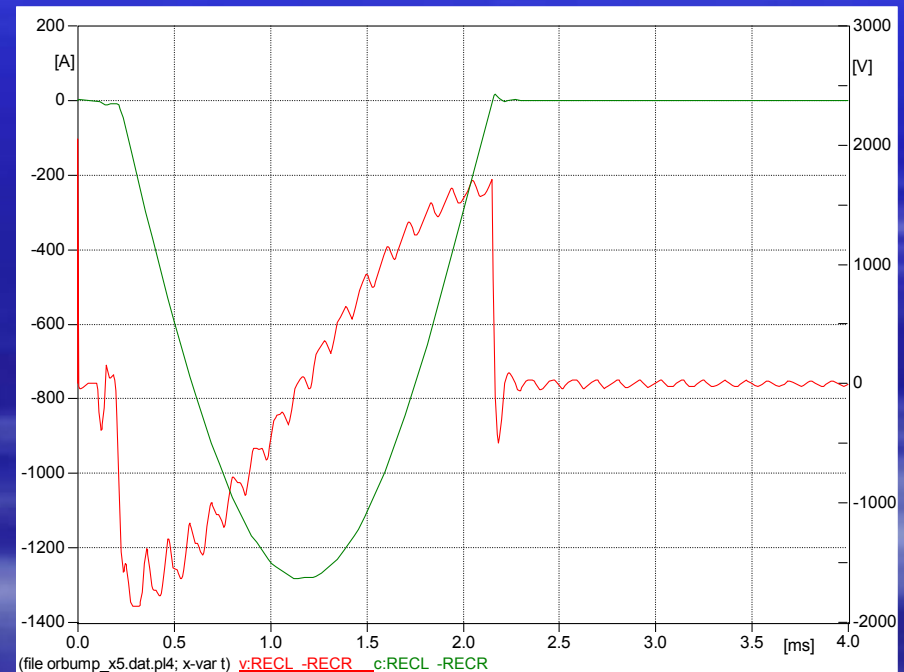
- $L = 0.8 \text{ mH}$

- $V = 2.2 \text{ kV}$

- Current

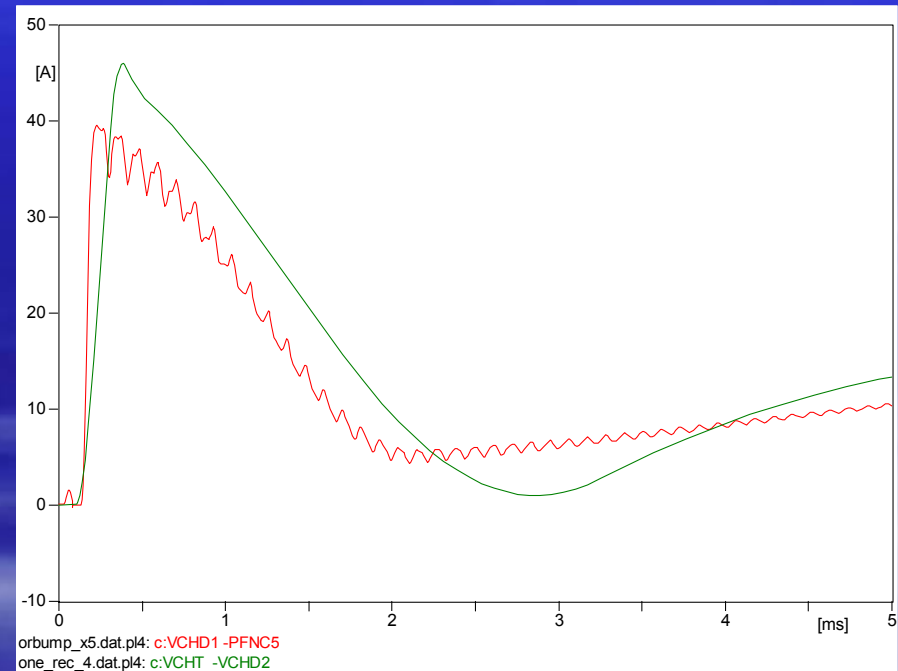
 - Peak = 2.5 kA

 - Rms = 400 A



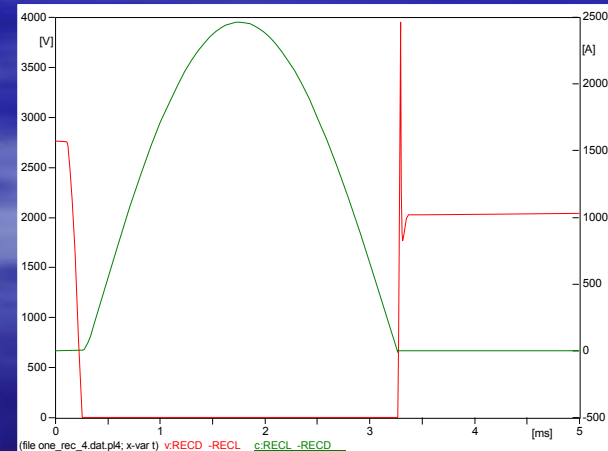
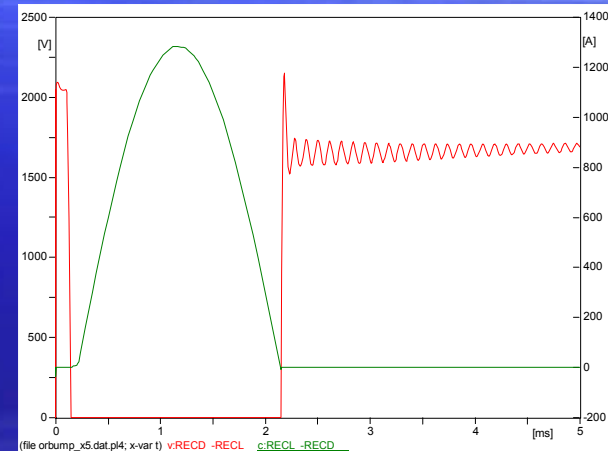
Charging Diodes

- Same as MP01/MP02 diodes
- Lower I_{\max} , I_{rms} , V_{\max}
- Same assembly as for charge recovery diodes

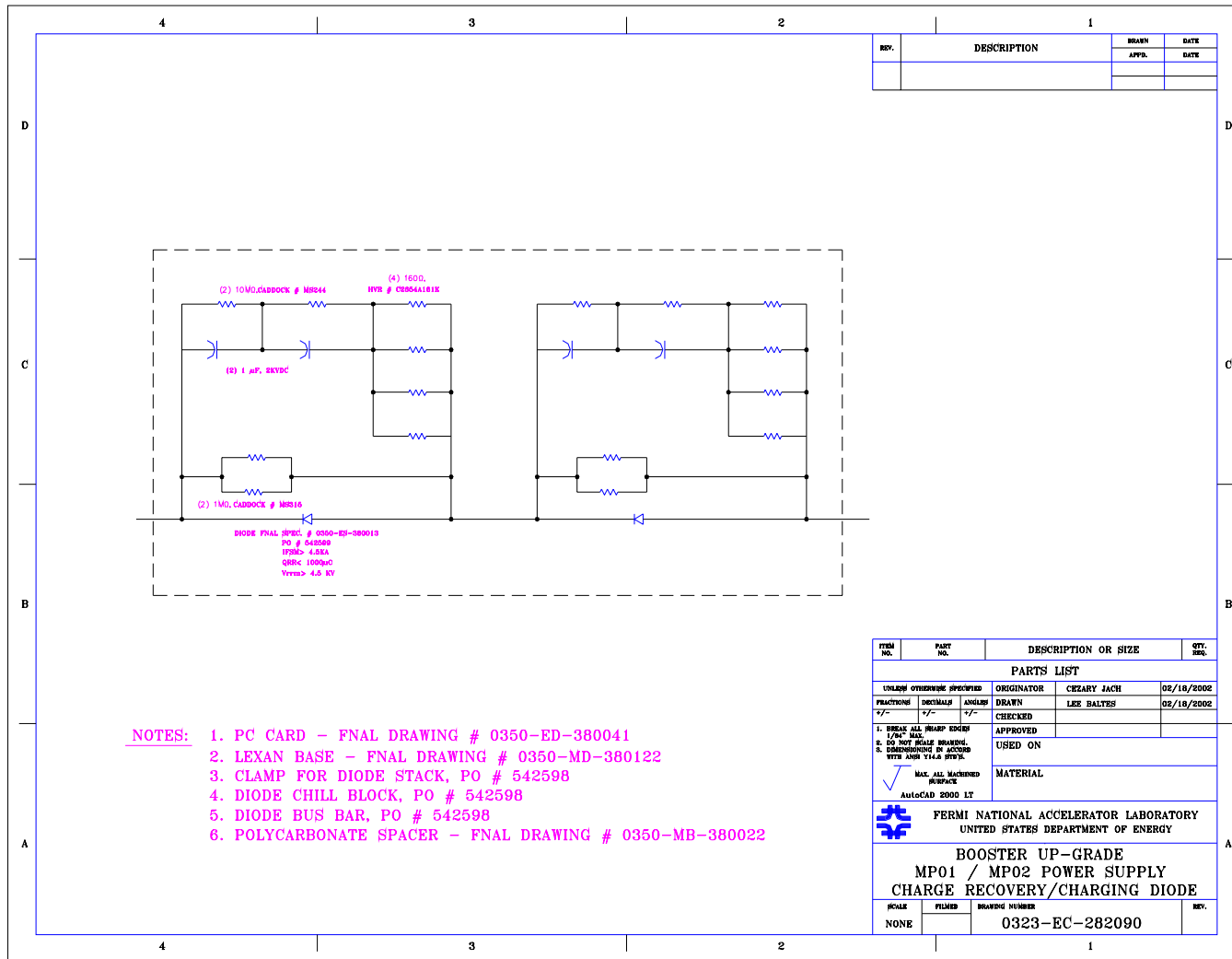


Charge Recovery Diodes

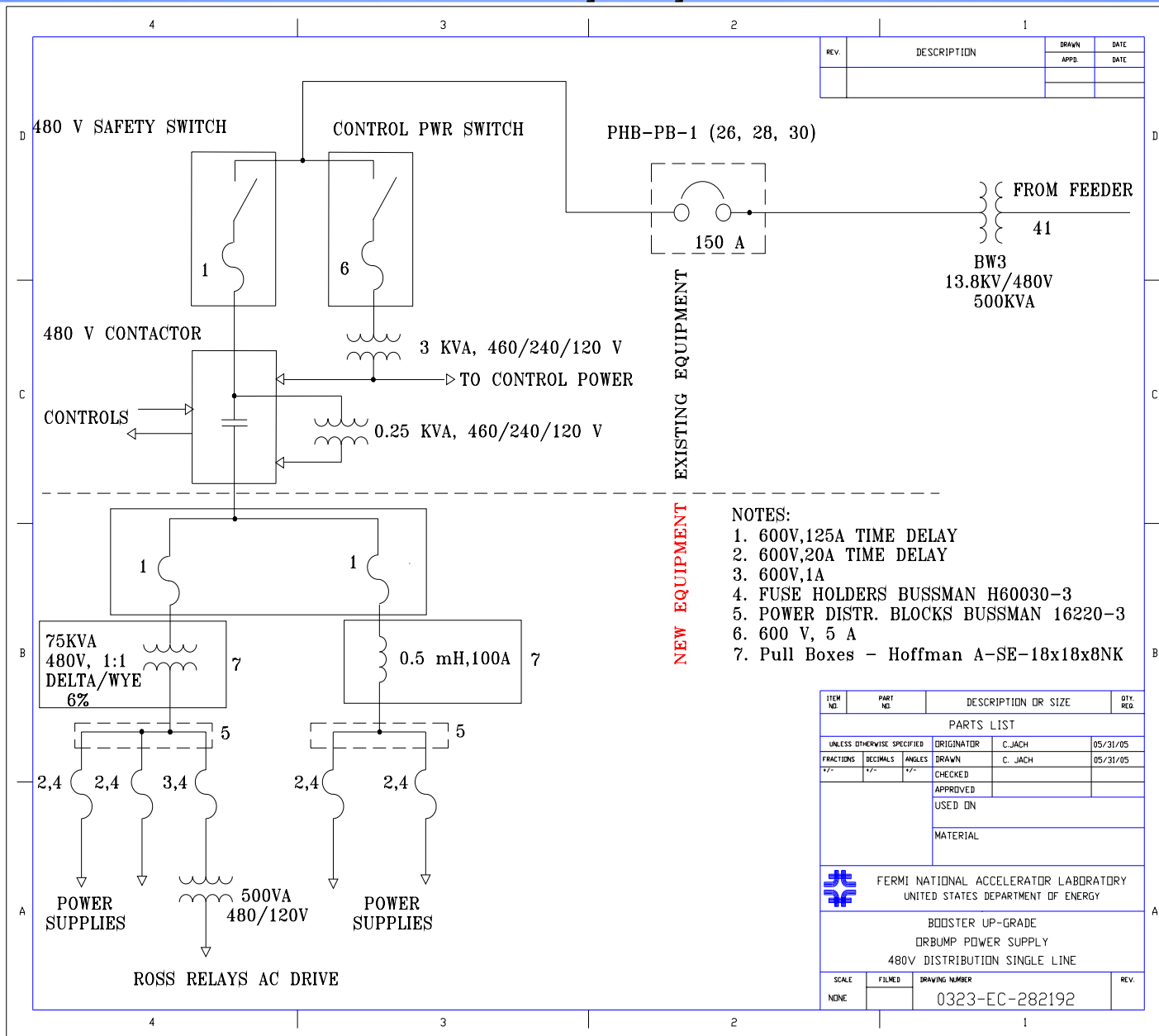
- ORBUMP Charge recovery diode
- MP01/MP02 Charge recovery diodes



Charging/Charge Recovery Diodes

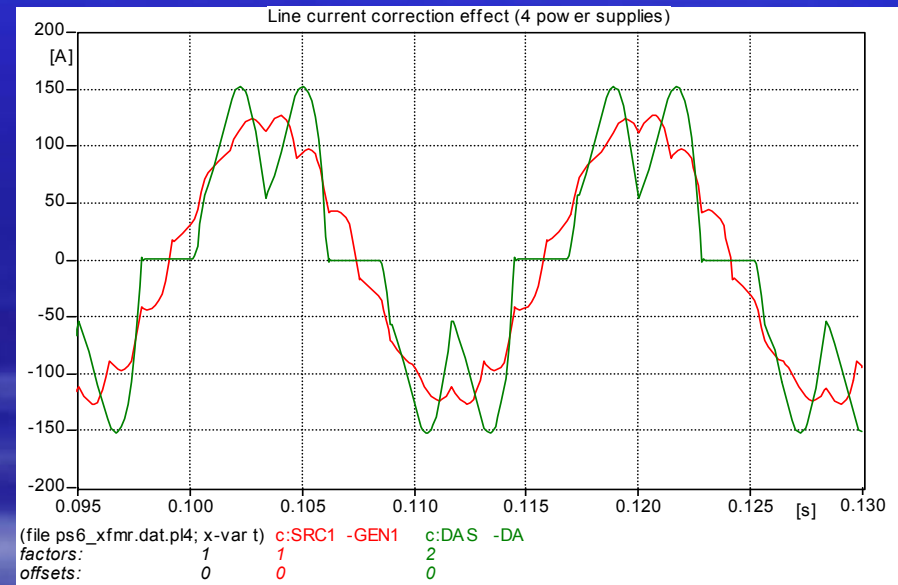


480 V Equipment



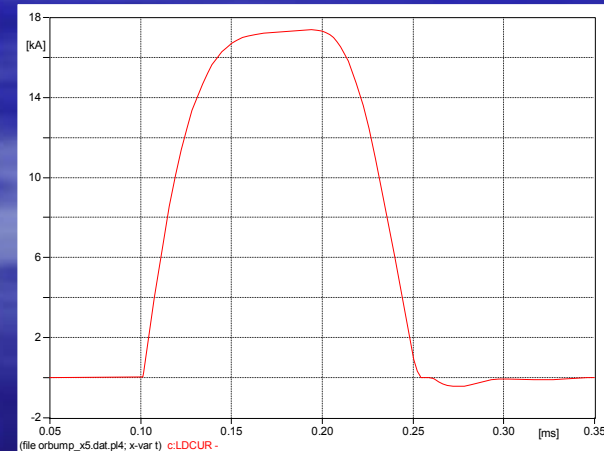
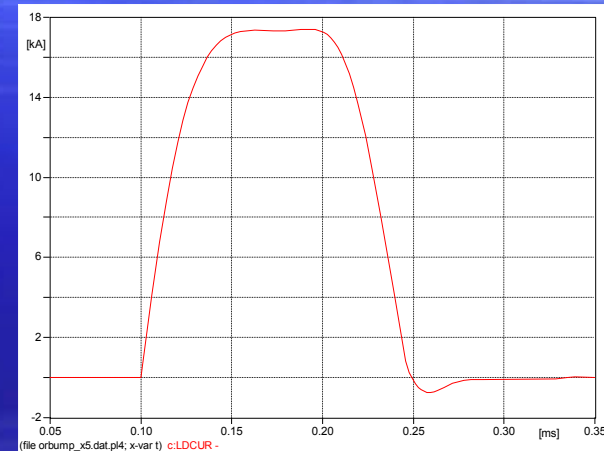
Line Harmonic Reduction

- Same system as for MP01 and MP02
- Effectively reduces current THD from 40% to 8%
- At 500 kVA transformer secondary voltage THD reduced from 19% to 1%



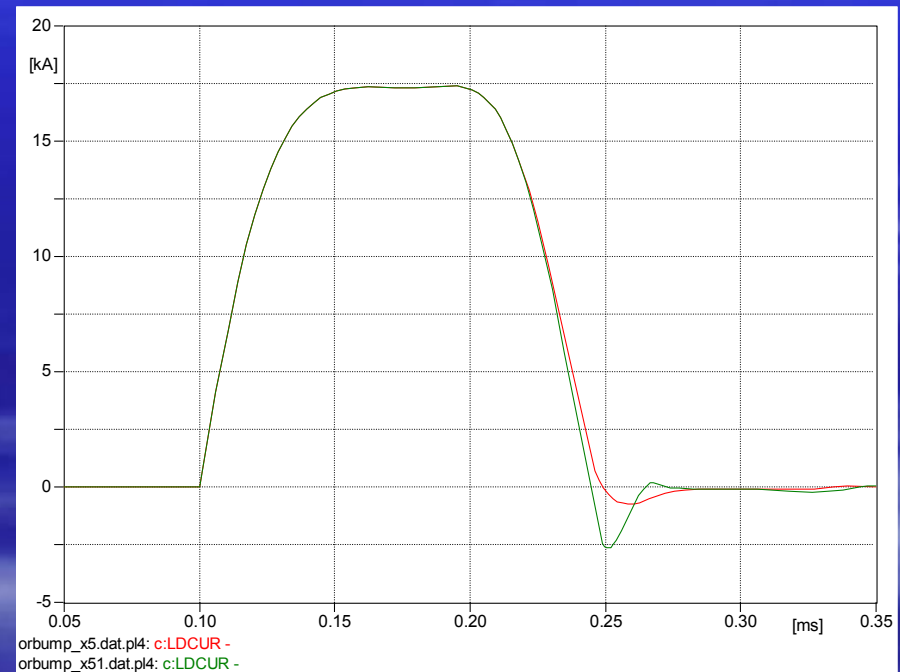
Is Saturating Inductor Needed?

- Without
 - $\text{Idot}_{\text{max}} = 700 \text{ A}/\mu\text{s}$
- Not Needed
- With:
 - $\text{Idot}_{\text{max}} = 600 \text{ A}/\mu\text{s}$



Is End-of-Pulse Clamp Needed?

- 4% vs. 15% undershoot
- Clamp is needed



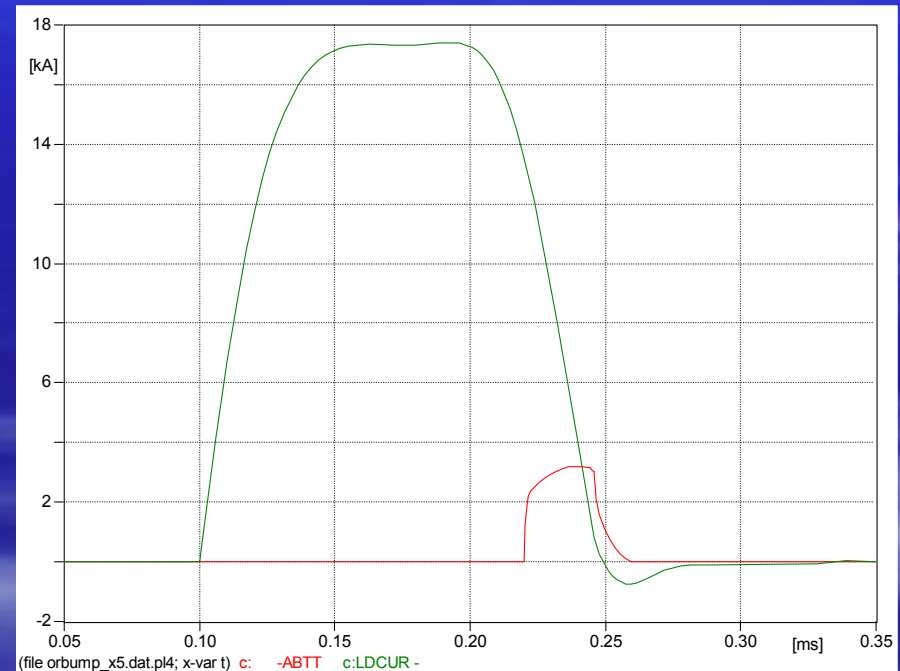
End-of-Pulse Clamp, cont.

■ Switch Parameters:

- $I_{\text{peak}} = 3200 \text{ A}$
- $I_{\text{ave}} = 2 \text{ A}$
- $I_{\text{rms}} = 80 \text{ A}$
- $T_{\text{conduction}} = 40 \mu\text{s}$
- $di/dt = 600 \text{ A}/\mu\text{s}$
- $V_{\text{peak}} = 2050 \text{ V}$

■ Design Concerns:

- Choice of SCR
- Snubber Design
- Trigger Design
- Timing

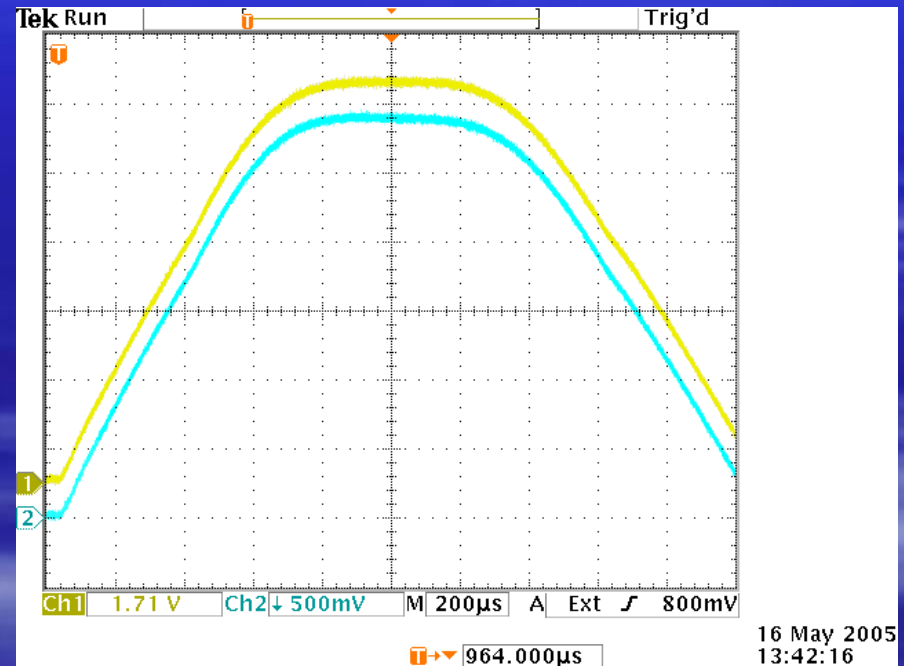


Monitoring - Current

- Pearson Model 1423
- Sensitivity = 0.001 V/A +1/-0%
- 15 V = 15 kA

Monitoring – SCR No Fire

- 5 LEM flex current probes
- Sensitivity 1 mV/A
- 3 kA = 3 V
- Tested at 300 A, 15 Hz



Voltage Monitoring

- Voltage divider Ross VDS-15-DH-K-FS
(same as MP01/MP02)
- 300:1
- $1800\text{ V} = 6\text{ V}$ (15 kA)

Energy Discharge

- Electronic Crowbar across a PFN capacitor in parallel with Ross relay
- Additional Ross relay across a PFN capacitor
- Ross Relay across charging power supplies (2 sec. delay)
- 200 k Ω bleeder resistors across capacitor (T= 100 sec.)

Safety Hazards

- The charging supplies are 3 kV dc and are powered from 480 V ac.
- Terminals for the capacitor bank (potentially 2.25 kJ, 1 kJ nominal) and high voltage bus (3 kV) are in the cabinet with 4 sets of double doors.

Hazard Mitigation

- All power for the system will come through a 480 V safety switch
- All doors in the power supply cabinet and equipment rack are interlocked to 480 V contactor
- Once 480 V power is removed, safety relays are dropped in; two across the capacitor bank, one (2 second delay) across the charging power supplies to prevent capacitor re-charging
- A resistive ground stick will be provided to accomplish the final grounding of the capacitor bank
- Visual inspection of the discharge resistors on relay assembly

Orbump Controls

Objective:

Use as much of MPO1/MPO2 controls as possible.

What can be used from MP01/MP02

- Contact Interface Card.
- Signal Interface Card.
- Timing & Control with timing mods.
- Peak Current Sample & Hold with timing mods.
- Cap Bank Voltage Regulator.
- Analog & Digital Feedback Cards.

What changes need to be made?

- The SCR Switch Current Monitor will need to be redone totally to monitor the 5 SCR Switch signals for a no-fire.
- The Load Current will come from a single CT, not a summation signal.
- The 118 Camac Module will need to be changed to a C217 module.
- A C284 Module will need to be added for more status readbacks.
- Timing Adjustments will need to be made for Peak sample & Hold.
- Minor Chassis wiring for above modifications.
- Charge/Fire Pulses ??
- Chassis Front Panel Display for 5 SCR Switch monitors.

Project Cost

- 106k\$ spent or committed
- 8k\$ estimated additional costs (electronics,, cables, buswork, supports, etc...)
- Does not include Ken's switch
- Does not include installation (electricians, riggers)

Project Labor Estimate (Lab)

- Does not include T&M
- Technicians
 - 13 man-months
- Engineers
 - 6 man-months total

Project Schedule

- All major parts are in-house. Capacitors are due at the end of August, but can be substituted if needed.
- Switch – 100% complete
- Power supply rack – 90% complete
- Controls rack – 50% complete
- Power supply cabinet – 0% complete

Spares

- Capacitors
 - 90 μF – 5 needed, 9 spares
 - 20 μF – 3 needed, 2 spares
- Charging Power Supplies – includes MP01/MP02
 - 10 needed, 3 spares
- Charging Chokes – includes MP01/MP02
 - 3 needed, 2 spares
- Charge Recovery Chokes – includes MP01/MP02
 - 3 needed, 2 spares
- Switch – 5 spare SCR assemblies
- All small parts have spares in various quantities

Documentation

- This document
- Power Supply Checkout (in preparation)
- Power Supply Power On (in preparation)
- Power Supply Scale Factors and Test Points (in preparation)
- Re-commissioning Plan (in preparation)
- LOTO document (in preparation)
- AUTOCAD schematics

Schematics

- ORBUMP Power Supply Block Diagram, FNAL drawing 0232-EC-282191
- ORBUMP 480 V Power Distribution Single Line Diagram, FNAL Drawing 0323-EC-282192
- Most MP01/MP02 schematics will apply
- Modifications and new schematics will be done if necessary